Separation of Oil-Water Emulsion in Laboratory Setup with U-Shaped Elements

Dang Vinh¹, Vadim Zinurov¹, Oksana Dmitrieva^{2,*}, and Vitaly Kharkov^{2,3}

¹Kazan State Power Engineering University, 420066, Krasnoselskaya street 51, Kazan, Russia
²Kazan National Research Technological University, 420015, Karl Marx street 68, Kazan, Russia
³Kazan National Research Technical University named after A. N. Tupolev - KAI, 420111, Karl Marx street 10, Kazan, Russia

Abstract. This study considers the problem of separation of oil-water emulsion in the case of oil spills. The standard methods of separation of the emulsion were presented. A unit with U-shaped separation elements has been developed. The device's operating principle was described, in which the separation of the oil-water emulsion occurs mainly due to the action of centrifugal forces arising from flow motion between the U-shaped elements and gravitational forces. The laboratory setup used for experiments was presented. The aim was to study the separation process of oil-water emulsion in a setup under varying initial temperature and initial density of the emulsion. The results showed that the device can separate the oil-water emulsion into light and heavy phases with an efficiency of at least 93.4% at a velocity of 1.39-2.15 m/s in narrow sections between the U-shaped elements. One way of improving the separation of the oil-water emulsion is to increase the working temperature. It was found that the increased efficiency of 2.5% indicates that device applicability caused the presence and availability of heating devices. As the crude oil content in the feed increases, it is necessary to increase the number of rows of U-shaped elements or repeat the process.

1 Introduction

Crude oil spills cause severe damage to aquatic ecosystems. Nowadays, an important task is to quickly and effectively clean-up contaminated waters from them because the consequences are tragic for natural processes, including changes in habitat conditions and losses for human society. Due to their lower density relative to water, oil products are floating on the surface of the sea or lake, forming an oil slick that changes the composition of the water and prevents the passage of oxygen through the oil layer, causing oxygen deficit. If water is not treated in the short term, then heavy oil products gradually begin to settle, contaminating benthal deposits. After a time, oil-water emulsions are formed, a separation of which becomes more difficult [1-3].

Moreover, oil products in water supply systems can have harmful economic, environmental, public health, and social effect. In particular, oil spills lead to a decrease in

^{*} Corresponding author: ja_deva@mail.ru

[©] The Authors, published by EDP Sciences. This is an open access article distributed under the terms of the Creative Commons Attribution License 4.0 (http://creativecommons.org/licenses/by/4.0/).

the population of diverse marine species, especially birds and marine invertebrates, mammals, to an increase in various diseases, including oncological and cardiovascular diseases in humans and other negative environmental consequences [4-7].

The challenge of primary importance when releasing oil products into freshwater or marine ecosystems is their localization. Containment booms or simply booms are ubiquitously used for this purpose [8], which typically come in three types:

- fence ones, as a rule, are utilized to reduce the possibility of polluting shorelines and nature protective zones;

- sorbent devices made of porous material, which absorbs the oil while it is being contained;

- inflatable booms made from a strong and high-visibility fabric are suitable for the initial oil slick containment.

Globally the following methods are common for removing oil from water [9, 10] thermal, mechanical, physicochemical, and biological. The thermal method consists of burning at the spill site or in the chamber, bubbler, rotary furnaces, etc. The mechanical method is a treatment of oil products by physical processes, from manual scooping to machine. The physicochemical method involves treating the oil layer with small thicknesses using surfactants (sorbents, dispersants, etc.). The biological method is based on the ability of some microorganisms to convert aromatic and aliphatic hydrocarbons into carbon dioxide and water. The capturing of oil products from the water surface is carried out by special technical devices – oil collectors, skimmers, which allow collecting the top layer of water with the oil for further clean-up.

The most promising method of clean-up water from oil products (separation of oil-water emulsion) is mechanical due to its low cost, high rate, and environmental friendliness compared with thermal methods. However, mechanical water treatment in most cases is preliminary since the efficiency varies in a wide range from 60 to 95%. Note that the mechanical method can only be a single operation when the cleaned water is dumped into the reservoirs without environmental disruption. In other cases, mechanical removal of oil from water should be combined with other methods [11-14].

The most common devices used for the mechanical treatment of water from oil products are settling tanks, hydrocyclones, filters, etc. The simplest and widely applied devices for wastewater treatment are settling tanks, which come in static, dynamic, thin-layer, tubular. Under the action of gravity, heavy impurities settle to the bottom, and the light ones float on its surface. The main drawbacks of the settling tanks are the low separation rate for oilwater emulsion and the vast footprint (it takes up much space). For example, when using static settling tanks, water treatment from oil products and other impurities is carried out periodically, and settling time is taken from 6 to 24 hours. Therefore, the oil-water emulsion settling tanks are used extremely rarely in oil spills. An operating principle of hydrocyclones involves an occurrence of centrifugal forces that act on oil droplets and throw them to the periphery of the device. Further, oil products are discharged through the lower outlet of the hydrocyclone. One of the main disadvantages of hydrocyclones is their low efficiency of about 70%.

Filters are the most effective devices for removing oil from water, based on the adhesion of coarse particles of oil products to the surface of the filter media. The main disadvantage of the filtration process is periodicity, as the filter elements are gradually contaminated and need to be replaced. Therefore, so far, an urgent task for cleaning up major oil spills is developing compact devices for separating oil-water emulsions with high efficiency [15-20].

To address this problem, a compact separation device with U-shaped elements was developed, which consists of an inlet 1 for oil-water emulsion supply, U-shaped elements 2, and holes for removal of oil products 3, a body 4, and an outlet 5 (Fig. 1). Notice that U-

shaped elements are positioned in staggered rows. At the same time, even rows of U-shaped elements can be cut in half to decrease in dimensions, which does not affect the flow pattern.

The operating principle of the separation device with U-shaped elements is as follows. Oil-water emulsion enters the device through inlet 1 and flows between rows of U-shaped elements 2. It is worth noting that the U-shaped elements are aligned with that when the liquid flows around them, centrifugal forces arise which acting on the flow and droplets, and the liquid is divided into two phases depending on their density, the oil components rush into the made holes. Often, the described process is disrupted since the centrifugal forces partially discard both the light and heavy phases, as a result of which the separation efficiency of the oil-water emulsion decreases.

In order to achieve the maximum centrifugal forces when the flow of liquid with oil components moves, it is necessary to fulfill the following structural condition: the auxiliary circle drawn from the center of the U-shaped element must pass through the extreme points of the protrusions of the U-shaped elements of neighboring rows. Thus, as the liquid with dispersed oil globules moves in the device, the oil fraction is separated by centrifugal and gravitational forces [21-24].





A primary task in developing a novel device for the oil-water emulsion separation is their study under changing parameters (technological, thermophysical, and others) and identifying the most promising ways for intensifying the water purification from oil products. Therefore, the work aims to study the separation process of oil-water emulsion in a laboratory setup with U-shaped elements.

2 Experimental methodology

The laboratory setup used in this study includes a disperser (1) and a mixing tank (2), a pump 3, an apparatus 4 with installed inside U-shaped separation elements 5 (Fig. 2).



Fig. 2. Laboratory test setup with U-shaped separation elements: 1 - disperser; 2 - mixing tank; 3 - pump; 4 - apparatus body; 5 - unit with U-shaped separation elements; 6 - holes of oil products discharge.

The experimental procedure was as follows. Water and oil were supplied into mixing tank 2, where using disperser 1, an oil-water emulsion was prepared. After mixing, the emulsion was pumped into apparatus 4. When the oil-water mixture enters the test unit with the U-shaped separation elements 5, the separation process into the different density phases occurs as described above. It should be noted that the part of the oil-water emulsion which exited through the middle section of the outlet pipe from test unit 5 returns to the emulsion preparation tank 2. A ball valve was used to control the flow rate of the oil-water emulsion.

During the experiments, the densities of the initial emulsion, light and heavy phases were being determined using the AM MDS-300 areometer, used to measure the density of oil products from 800 to 1010 kg/m³. The average weight flow ratio of heavy and light phases was 1:10. The velocity of the oil-water emulsion in the narrow sections of the unit with U-shaped separation elements was from 1.39 to 2.15 m/s. The initial temperature of the oil-water emulsion was 30°C. The basic physicochemical properties of the crude oil used in the experiments are listed in Table 1. The crude oil used in the studies had a high freezing point, about 33°C, the content of solid paraffin in crude oil was 27%, the melting point of solid paraffin was in the range from 50 to 65°C.

Parameter	Crude oil	Test method
API	38.6	ASTM D 1298–96
Freezing point, °C	33	ASTM D 97; ASTM D 6749-02
Kinematic viscosity at 40 °C, cSt	10	ASTM D 445
Paraffin content, mass%	27	GOST 11858–85
Asphaltenes content, mass%	0.77	GOST 1185-85 (ASTM D 6560)
Molecular weight, g/mol	392	ASTM D 2502
Acid number, mg KOH/g	0.04	ASTM D 664-89 (ASTM D 664)
Water content, mass%	12	ASTM D 95; (ASTM D 1744)

Table 1. Chemical & Physical Properties of Crude Oil.

The effect of the content of the crude oil in the feed tank 2 and the temperature which varied from 30 to 75 °C on the separation efficiency E was examined by the following equation:

$$E = \frac{\overline{x_D} - \overline{x_F}}{1 - \overline{x_F}},\tag{1}$$

where $\overline{x_D}$ is the mass fraction of oil in the light phase, kg/kg; $\overline{x_F}$ is the mass fraction of oil in the feed emulsion, kg/kg.

3 Results and discussion

The results show that the device with U-shaped elements can separate oil-water emulsion with the efficiency in the range of 96.4–98.8% at an initial temperature of $30-75^{\circ}C$ and an initial density of 848–996 kg/m³, as shown in Fig. 3–4. A high velocity of oil-water emulsion flow inside the unit with separation elements – averaged value was of 1.7 m/s at narrow sections between U-shaped elements. High velocities produced high centrifugal forces that lead to the formation of stable swirls at the round holes 3 (Fig. 1), resulting in an increase in the separation efficiency of the oil-water emulsion into light and heavy phases. The increase in the temperature of the feed emulsion promotes the separation process. At higher temperatures, the viscosity of the emulsion decreases, increasing the density difference between water and crude oil.



Fig. 3. Influence of initial temperature on separation efficiency.

It should be noted that with a rise in the temperature of the oil-water emulsion, the surface strength of the oil globules also decreases; as a consequence, their coalescence occurs. However, if this method is combined with chemical one, more additional research needs to be carried out since some demulsifiers are effective only at low temperatures, others only at high temperatures. The minimum separation efficiency of the oil-water emulsion was 96.4% at a feed temperature of 30°C. As the temperature rises from 30 to 50°C, the efficiency magnifies by 2.4%. The constant separation efficiency of 98.8% was

observed at a temperature above 50 °C. The increase in the efficiency of the emulsion separation at temperatures of 30–75 °C does not exceed 2.5%, so this method can be recommended. Besides, when the temperature falls below 30 °C, there can be a significant decrease in the separation efficiency of the oil-water emulsion (Fig. 3).

An increase in the crude oil content in the feed promotes the growth of the density of the oil-water emulsion from 848 to 996 kg/m³, causing a decrease in its separation efficiency from 98.8 to 93.4%. The maximum separation efficiency is 98.8% when the density of the oil-water emulsion changes from 848 to 892 kg/m³. The considerable decrease in emulsion separation efficiency from 98.8 to 93.7% occurs when its initial density varies from 892 to 976 kg/m³. With an initial emulsion density of 976–996 kg/m³, the separation efficiency is 93.5%. At high oil content, the decline in the separation efficiency of the emulsion is observed, as some amount of the fractions are mixed again at the places of formation of swirls (near round holes). In order to improve efficiency, it is necessary to increase the number of rows of U-shaped elements (Fig. 4).





Thus, studies have shown that using the developed unit with U-shaped separation elements is a cost-efficient clean-up method for oil spills due to the high efficiency, compactness design, simplicity in operation, and the absence of moving parts. One promising way of improving the separation of the oil-water emulsion is to increase the working temperature. However, from obtained results, it is clear that the increased efficiency of $\pm 2.5\%$ indicates that device applicability caused the presence and availability of heating devices. As the crude oil content in the feed increases, it is necessary to increase the number of rows of U-shaped elements or repeat the process.

4 Conclusions

The following conclusions can be drawn from the study:

- the design of the separation device with the U-shaped elements has been developed, that provides the separation of the oil-water emulsion with the efficiency of more than 93.4% at its velocities from 1.39 to 2.15 m/s in the narrow sections between the U-shaped elements;

- the separation process of the oil-water emulsion is mainly performed due to the action of centrifugal forces arising from the flow motion between the U-shaped elements;

– increase in the separation efficiency of the oil-water emulsion to 98.8% with increasing the temperature to 50° C;

- reduction in the separation efficiency with increasing the concentration of crude oil in the feed mixture. When the density of the initial mixture varies from 848 to 996 kg/m³, the separation efficiency decreases from 98.8 to 93.4% due to secondary mixing along the height of the device, where round holes are made;

- the main benefits of the developed separator with the U-shaped elements are compactness, high efficiency, and low operating costs.

The reported study was funded by the grant of the President of the Russian Federation, project number MK-616.2020.8.

References

- 1. M. D'Andrea and K. Reddy, Am. J. Med., 127 (2014).
- 2. G. M. Solomon and S. Janssen, JAMA, **304**, 1118 (2010).
- 3. S. E. Chang, J. Stone, K. Demes, and M. Piscitelli, Ecol. Soc., 19, 26 (2014).
- 4. J. W. Farrington, Mar. Pollut. Bull., 150, 110744 (2020).
- 5. M. Lee, M. S. Park, and H. K. Cheong, Ecotoxicol. Environ. Saf., 194, 110284 (2020).
- 6. K. A. Colvin, C. Lewis, and T. S. Galloway, Chemosphere, 245, 125585 (2020).
- 7. F. Aguilera, J. Mendez, E. Pásaro, and B. Laffon, J. Appl. Toxicol., 30, 291 (2010).
- 8. M. Fingas, in (2021), pp. 875–889.
- 9. O. A. Johnson and A. C. Affam, Environ. Eng. Res., 24, 191 (2019).
- 10. A. Hoang, X. P. Nguyen, X.-Q. Duong, and T. Huynh, Environ. Sci. Pollut. Res., (2021).
- 11. R. K. Gupta, G. J. Dunderdale, M. W. England, and A. Hozumi, J. Mater. Chem. A, 5, 16025 (2017).
- 12. K. Wang, W. Yiming, J. Saththasivam, and Z. Liu, Nanoscale, 9, 9018 (2017).
- 13. A. Cambiella, J. M. Benito, C. Pazos, and J. Coca, Chem. Eng. Res. Des., 84, 69 (2006).
- A. Dmitriev, V. Zinurov, O. Dmitrieva, and V. Dang Xuan, Her. Kazan State Power Eng. Univ., 3 (39), 65 (2018).
- 15. Q. Zeng, Z. Wang, X. Wang, Y. Zhao, and X. Guo, J. Pet. Sci. Eng., 145, 83 (2016).
- A. Dmitriev, V. Zinurov, D. Vinh, and O. Dmitrieva, E3S Web Conf., 110, 1026 (2019).
- 17. X. Zeng, L. Zhao, G. Fan, and C. Yan, Chem. Eng. Res. Des., 165, 308 (2021).
- S. Y. Shi, J. Y. Xu, H. Q. Sun, J. Zhang, D. H. Li, and Y. X. Wu, Chem. Eng. Res. Des., 90, 1652 (2012).
- 19. I. Madyshev, I. Sabanaev, V. Kharkov, L. Ganiev, and A. Dmitriev, MATEC Web Conf., **329**, 3007 (2020).

- 20. J. J. Slot, Development of a Centrifugal In-Line Separator for Oil-Water Flows, University of Twente, 2013.
- 21. O. S. Popkova, W. L. Nguyen, O. S. Dmitrieva, I. N. Madyshev, and A. N. Nikolaev, J. Phys. Conf. Ser., **1210**, 012114 (2019).
- 22. V. V. Kharkov, J. Phys. Conf. Ser., 980, 012006 (2018).
- 23. A. V. Dmitriev, V. E. Zinurov, and O. S. Dmitrieva, MATEC Web Conf., **224**, 02073 (2018).
- 24. V. E. Zinurov, N. Z. Dubkova, O. S. Popkova, and O. S. Dmitrieva, J. Phys. Conf. Ser., 1745, 012090 (2021).